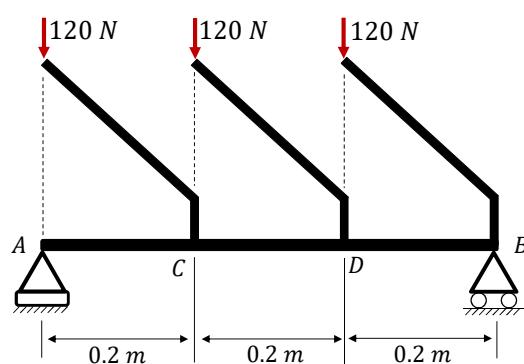


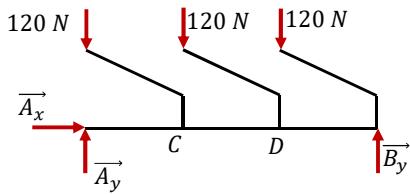
ME201 – Statics

Chapter 7&8 – Recitation 06

Example 1



Draw the shear force and bending moment diagrams for the beam AB.



$$(\curvearrowleft+) \sum \vec{M}_A = 0$$

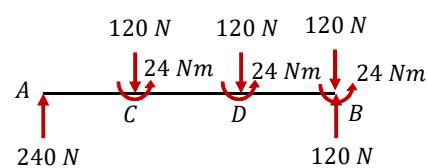
$$-120 \times 0.2 - 120 \times 0.4 - B_y \times 0.6 = 0$$

$$B_y = 120 \text{ N} (\uparrow)$$

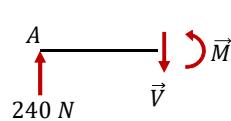
$$(\uparrow+) \quad \sum \vec{F}_y = 0 \qquad (\rightarrow+) \quad \sum \vec{F}_x = 0$$

$$-360 + A_y + 120 = 0 \qquad A_x = 0$$

$$A_y = 240 \text{ N} (\uparrow)$$



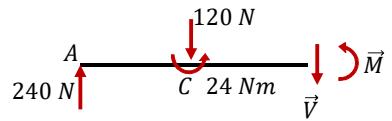
Between A – C



$$\vec{V} = 240 \text{ N}$$

$$\vec{M} = 240x$$

Between C – D

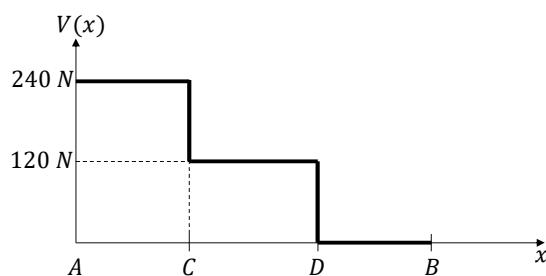
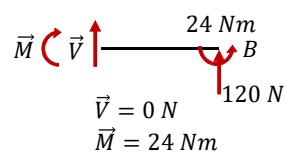


$$\vec{V} = 120 \text{ N}$$

$$\vec{M} - 240x + 120(x - 0.2) + 24 = 0$$

$$\vec{M} = 120x$$

Between D - B



$M(x)$

48 Nm

24 Nm

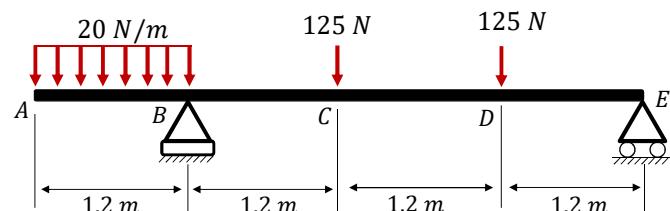
A

C

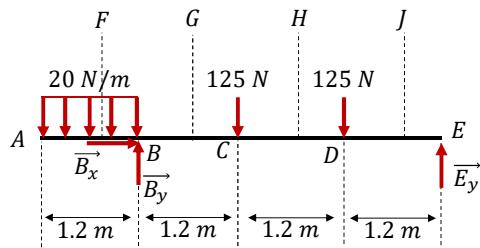
D

B

Example 2



Draw the shear force and bending moment diagrams for the beam AE.

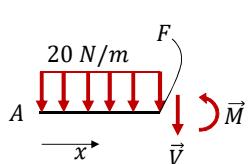


$$\begin{aligned}
 (\textcirclearrowleft+) \sum \vec{M}_B &= 0 \\
 -125 \times 1.2 - 125 \times 2.4 - E_y \times 3.6 + (20 \times 1.2) \times 0.6 &= 0 \\
 E_y &= 121 \text{ N } (\uparrow)
 \end{aligned}$$

$$\begin{aligned}
 (\uparrow+) \sum \vec{F}_y &= 0 \\
 -24 + B_y - 125 - 125 + 121 &= 0 \\
 B_y &= 153 \text{ N } (\uparrow)
 \end{aligned}$$

$$B_x = 0$$

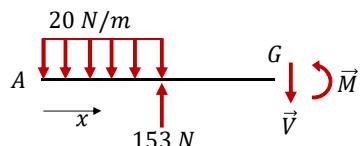
A - B @ F



$$\begin{aligned}
 (\uparrow+) \sum \vec{F}_y &= 0 & V(x=0) &= 0 \\
 V + 20x &= 0 & V(x=1.2) &= -24 \text{ N} \\
 \boxed{V = -20x}
 \end{aligned}$$

$$\begin{aligned}
 (\textcirclearrowleft+) \sum \vec{M}_F &= 0 & M(x=0) &= 0 \\
 M + 20x \frac{x}{2} &= 0 & M(x=1.2) &= -14.4 \text{ Nm} \\
 \boxed{M = -10x^2}
 \end{aligned}$$

B - C @ G



$$\begin{aligned}
 (\uparrow+) \sum \vec{F}_y &= 0 \\
 V + 20 \times 1.2 - 153 &= 0 \\
 \boxed{V = 129 \text{ N}}
 \end{aligned}$$

$$\begin{aligned}
 (\textcirclearrowleft+) \sum \vec{M}_G &= 0 \\
 M + (20 \times 1.2)(x - 0.6) - 153 \times (x - 1.2) &= 0 \\
 \boxed{M = 129x - 169.2} \\
 M(x=1.2) &= -14.4 \text{ Nm} \\
 M(x=2.4) &= 140.4 \text{ Nm}
 \end{aligned}$$

C - D @ H

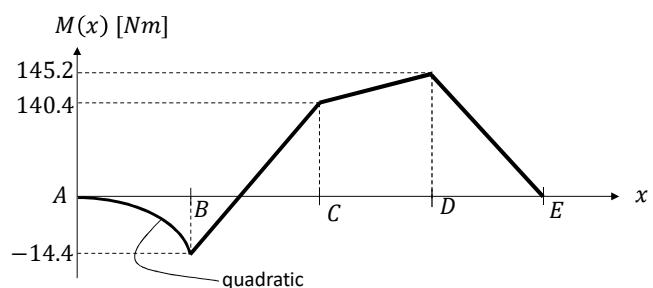
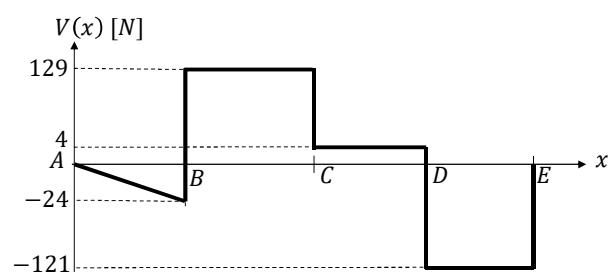
$$\begin{aligned} &(\uparrow+) \sum \vec{F}_y = 0 \\ &V + 20 \times 1.2 - 153 + 125 = 0 \\ &\boxed{V = 4 \text{ N}} \\ &(\curvearrowright+) \sum \vec{M}_H = 0 \\ &M + (20 \times 1.2)(x - 0.6) - 153 \times (x - 1.2) \\ &+ 125 \times (x - 2.4) = 0 \\ &\boxed{M = 4x - 130.8} \end{aligned}$$

$$\begin{aligned} M(x = 2.4) &= 140.4 \text{ Nm} \\ M(x = 3.6) &= 145.2 \text{ Nm} \end{aligned}$$

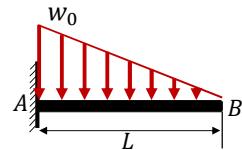
D - E @ J

$$\begin{aligned} &(\uparrow+) \sum \vec{F}_y = 0 \\ &V + 121 = 0 \\ &\boxed{V = -121 \text{ N}} \\ &(\curvearrowright+) \sum \vec{M}_J = 0 \\ &M - 121 \times (4.8 - x) = 0 \\ &\boxed{M = 580.8 - 121x} \end{aligned}$$

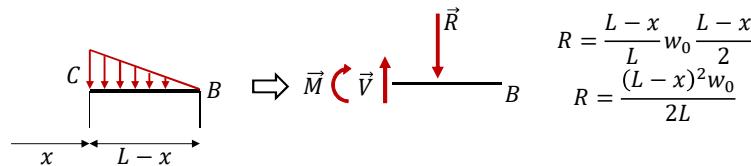
$$\begin{aligned} M(x = 3.6) &= 145.2 \text{ Nm} \\ M(x = 4.8) &= 0 \text{ Nm} \end{aligned}$$



Example 3



Draw the shear force and bending moment diagrams for the beam AB.



$$R = \frac{L-x}{L} w_0 \frac{L-x}{2}$$

$$R = \frac{(L-x)^2 w_0}{2L}$$

$$(\uparrow +) \sum \vec{F}_y = 0$$

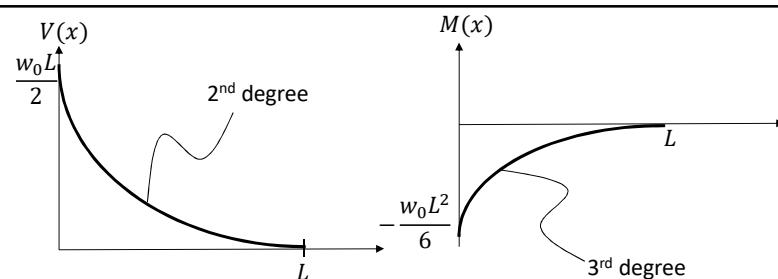
$$-\frac{(L-x)^2 w_0}{2L} + V = 0$$

$$V = \frac{(L-x)^2 w_0}{2L}$$

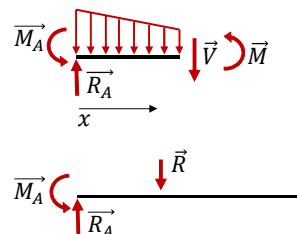
$$(\curvearrowright +) \sum \vec{M}_c = 0$$

$$\frac{L-x}{3} \times \frac{(L-x)^2 w_0}{2L} + M = 0$$

$$M = -w_0 \frac{(L-x)^3}{6L}$$



One can solve the problem considering the left portion of the beam as well.

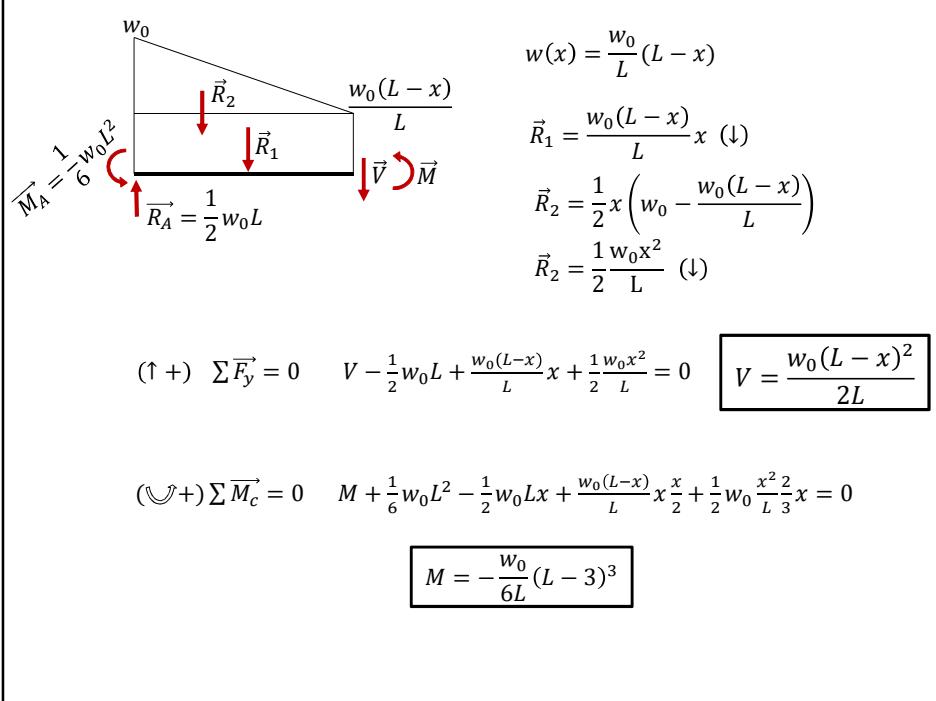


First determine the reactions.

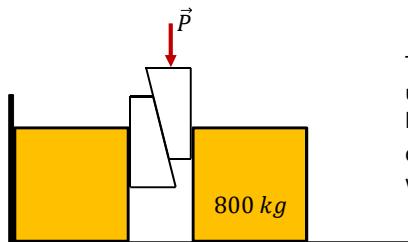
$$(\uparrow +) \sum \vec{F}_y = 0 \quad (\curvearrowright +) \sum \vec{M}_A = 0$$

$$R_A - \frac{1}{2} L w_0 = 0 \quad (\uparrow) \quad -\frac{1}{3} L \times \frac{1}{2} L w_0 + M_A = 0$$

$$R_A = \frac{1}{2} L w_0 \quad M_A = \frac{1}{6} w_0 L^2 \quad (\curvearrowright)$$



Example 4

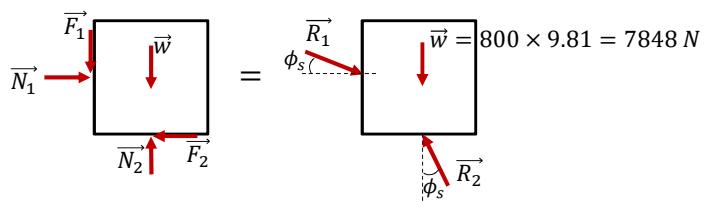


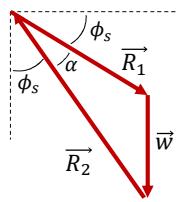
Two 8° wedges of negligible weight are used to move and position the 800 kg block. $\mu_s = 0.25$ at all surfaces of contact. Determine the smallest force \vec{P} which should be applied as shown.

$$\mu_s = 0.25$$

$$\phi_s = \tan^{-1}(\mu_s) = 14.04^\circ$$

FBD of the block



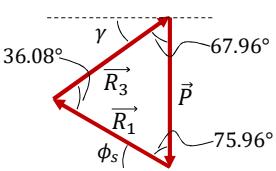
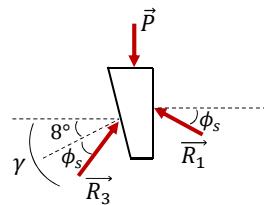


$$\alpha = 90 - 2\phi_s = 90 - 2 \times 14.04 = 61.92^\circ$$

Law of sines

$$\frac{R_1}{\sin \phi_s} = \frac{w}{\sin \alpha} \quad R_1 \approx 2158 \text{ N}$$

FBD of the wedge



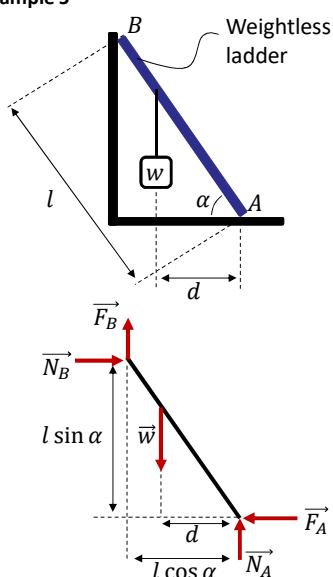
Law of sines

$$\frac{P}{\sin 36.08} = \frac{R_1}{\sin 67.96}$$

$$P = 1371 \text{ N} (\downarrow)$$

One can solve the same problem by considering the FBD of 800 kg block & the wedge and writing $\sum F_x = 0$ & $\sum F_y = 0$.

Example 5



What is the maximum value of d in terms of μ_s , l and α ? μ_s is the same for both surfaces.

$$F_A = \mu_s N_A$$

$$F_B = \mu_s N_B$$

$$(\uparrow +) \quad \sum \vec{F}_y = 0 \quad F_B + N_A - w = 0$$

$$w = N_A + \mu_s N_B \quad (1)$$

$$(\rightarrow +) \quad \sum \vec{F}_x = 0 \quad N_B - F_A = 0$$

$$N_B = \mu_s N_A \quad (2)$$

$$\begin{aligned}
 (\textcircled{J}+) \sum \overrightarrow{M_A} &= 0 \\
 wd - N_B l \sin \alpha - F_B l \cos \alpha &= 0 \\
 wd &= N_B l \sin \alpha - \mu_s N_B l \cos \alpha
 \end{aligned}$$

$$d = \frac{N_B l (\sin \alpha + \mu_s \cos \alpha)}{w} \quad (3)$$

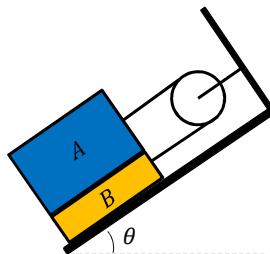
$$(2) \rightarrow (1) \quad \mu_s N_B + \frac{1}{\mu_s} N_B = w$$

$$w = N_B \left(\frac{1 + \mu_s^2}{\mu_s} \right) \quad (4)$$

$$(4) \rightarrow (3) \quad \mu_s N_B + \frac{1}{\mu_s} N_B = w$$

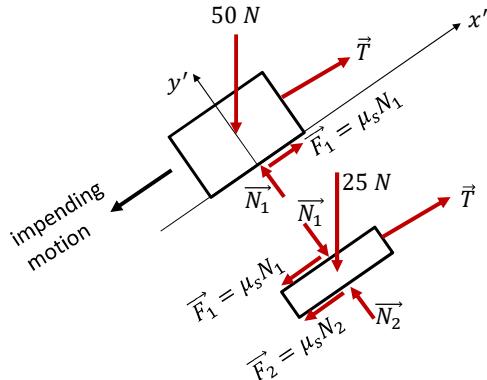
$$d = \frac{\mu_s l (\sin \alpha + \mu_s \cos \alpha)}{1 + \mu_s^2}$$

Example 6



Block A weights 50 N and block B weights 25 N. Knowing that the coefficient of static friction is 0.15 between all surfaces of contact, determine the value of θ for which the motion is impending.

A direction of impending motion should be selected.



FBD of block A

$$(\wedge+) \quad \sum \vec{F}_{y'} = 0 \quad N_1 - 50 \cos \theta = 0 \quad N_1 = 50 \cos \theta \quad (1)$$

$$(\nearrow+) \quad \sum \vec{F}_{x'} = 0 \quad T + F_1 - 50 \sin \theta = 0$$

$$T = -F_1 + 50 \sin \theta \quad (2)$$

$$F_1 = \mu_s N_1 = 0.15(50 \cos \theta) = 7.5 \cos \theta$$

Substitute into (2)

$$T = 50 \sin \theta - 7.5 \cos \theta \quad (3)$$

FBD of block B

$$(\nwarrow+) \quad \sum \vec{F}_{y'} = 0 \quad N_2 - N_1 - 25 \cos \theta = 0$$

Substitute N_1 from (1)

$$N_2 = 75 \cos \theta \quad (4)$$

$$(\nearrow+) \quad \sum \vec{F}_{x'} = 0$$

$$T - F_1 - F_2 - 25 \sin \theta = 0$$

$$F_2 = 0.15(75 \cos \theta) = 11.25 \cos \theta$$

$$T = 25 \sin \theta + 18.75 \cos \theta \quad (5)$$

By equating (3) and (5)

$$50 \sin \theta - 7.5 \cos \theta = 25 \sin \theta + 18.75 \cos \theta$$

$$\tan \theta = \frac{26.25}{25}$$

$$\theta \approx 46.4^\circ$$

If the opposite direction is chosen.

FBD of block A

$$(\nwarrow+) \quad \sum \vec{F_{y'}} = 0 \quad N_1 - 50 \cos \theta = 0 \quad \boxed{N_1 = 50 \cos \theta} \quad (1)$$

$$(\nearrow+) \quad \sum \vec{F_{x'}} = 0 \quad T - F_1 - 50 \sin \theta = 0$$

$$\boxed{T = 7.5 \cos \theta + 50 \sin \theta} \quad (2)$$

FBD of block B

$$(\nwarrow+) \quad \sum \vec{F_{y'}} = 0 \quad N_2 - N_1 - 25 \cos \theta = 0 \quad (\nearrow+) \quad \sum \vec{F_{x'}} = 0 \\ T + F_1 + F_2 - 25 \sin \theta = 0 \\ T + 7.5 \cos \theta + 11.25 \cos \theta - 25 \sin \theta = 0$$

$$\boxed{N_2 = 75 \cos \theta} \quad (3)$$

$$\boxed{T = 25 \sin \theta - 18.75 \cos \theta} \quad (4)$$

By equating (2) and (5) $7.5 \cos \theta + 50 \sin \theta = 25 \sin \theta - 18.75 \cos \theta$

$$\tan \theta = -\frac{26.25}{25}$$

$$\boxed{\theta \approx -46.4^\circ} \quad \text{Does not make sense!}$$